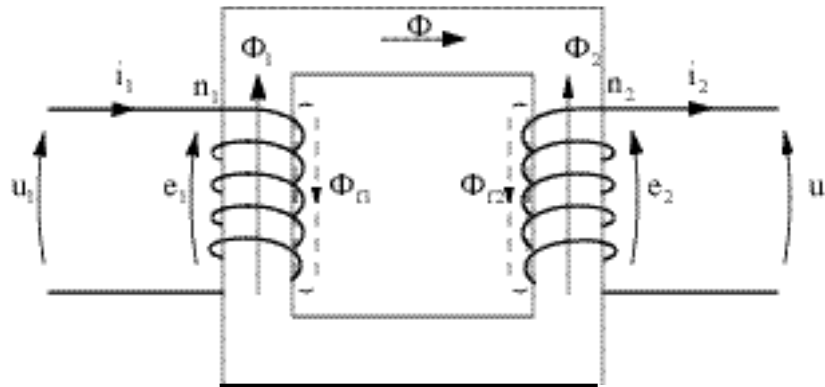


Single-phase transformer

2 windings (primary & secondary) around a magnetic core (magnetic coupling)

Faraday's law



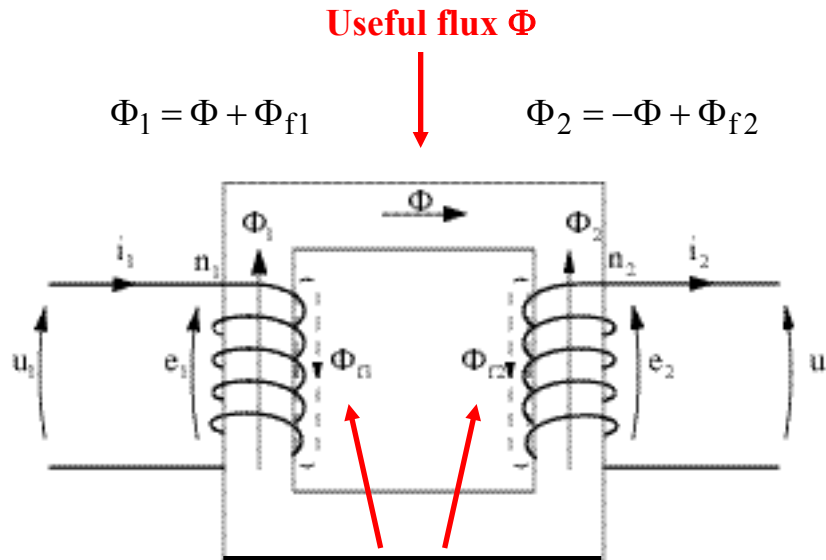
A time-dependent (varying) magnetic flux density in the magnetic core induces (time-dependent) electromotive forces (e.m.f.s) in each winding

The voltage in each winding (\sim) is proportional to the number of turns

Open or closed secondary ...

Electric energy conversion from one voltage level to another

General transformer relations



Useful flux Φ

$$\Phi_1 = \Phi + \Phi_{f1}$$

$$\Phi_2 = -\Phi + \Phi_{f2}$$

Leakage flux

$$\Phi_{f1} = \frac{n_1 i_1}{R_{f1}} \quad \text{et} \quad \Phi_{f2} = \frac{n_2 i_2}{R_{f2}}$$

Leakage reluctances

$$\frac{e_1}{n_1} = \frac{e_2}{n_2} = n$$

Transformation ratio

Primary winding equation

$$u_1 = R_1 i_1 + n_1 \partial_t \Phi_1 = R_1 i_1 + n_1 \partial_t \Phi_{f1} + n_1 \partial_t \Phi$$

$$u_1 = R_1 i_1 + \lambda_1 \partial_t i_1 + e_1$$

e.m.f in 1 due to Φ

Secondary winding equation

$$u_2 = -R_2 i_2 - n_2 \partial_t \Phi_2 = -R_2 i_2 - n_2 \partial_t \Phi_{f2} + n_2 \partial_t \Phi$$

$$u_2 = -R_2 i_2 - \lambda_2 \partial_t i_2 + e_2$$

e.m.f. in 2 due to Φ

Coupling equation

$$\Phi = \frac{n_1 i_1 - n_2 i_2}{R}$$

Magnetic circuit reluctance

$$e_1 = \frac{n_1^2}{R} \left(\partial_t i_1 - \frac{n_2}{n_1} \partial_t i_2 \right)$$

magnetizing inductance λ_μ

Transformer equivalent circuit

$$u_1 = R_1 i_1 + \lambda_1 \partial_t i_1 + e_1 \quad (a)$$

$$u_2 = -R_2 i_2 - \lambda_2 \partial_t i_2 + e_2$$

$$\frac{e_1}{e_2} = \frac{n_1}{n_2} = n$$

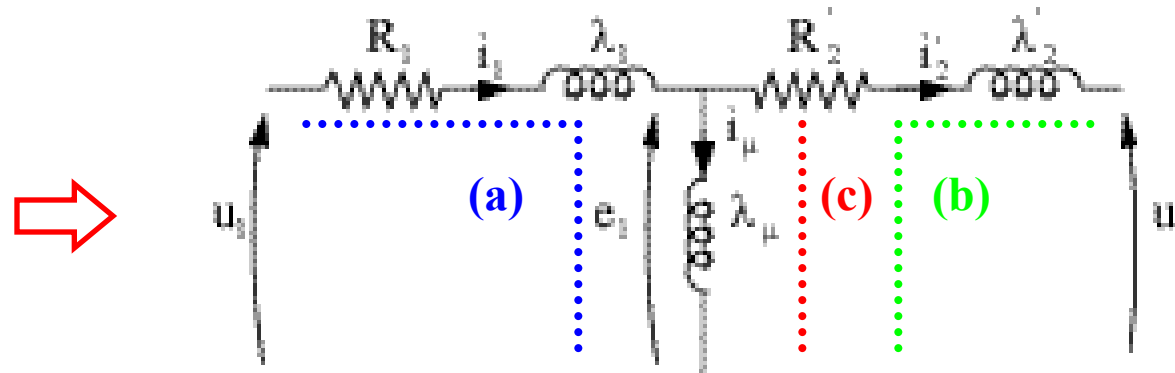
$$e_1 = \lambda_\mu \left(\partial_t i_1 - \frac{n_2}{n_1} \partial_t i_2 \right)$$

$$e_1 = n u_2 + n^2 R_2 \frac{1}{n} i_2 + n^2 \lambda_2 \frac{1}{n} \partial_t i_2$$

Secondary quantities as seen from the primary

$$e_1 = u'_2 + R'_2 i'_2 + \lambda'_2 \partial_t i'_2 \quad (b)$$

$$e_1 = \lambda_\mu (\partial_t i_1 - \partial_t i'_2) \quad (c)$$



Complex formalism: phasors

Complex representation of sinusoidal quantities

$$a(t) = A \cos(\omega t + \varphi)$$

*Sinusoidal quantity
(voltage, current, ...)*

- A maximum value (amplitude) of $a(t)$ [V, A, ...]
- ω pulsation of $a(t)$ ($2\pi f$, f = frequency) [rad/s]
- φ phase of $a(t)$ at $t = 0$ [rad]

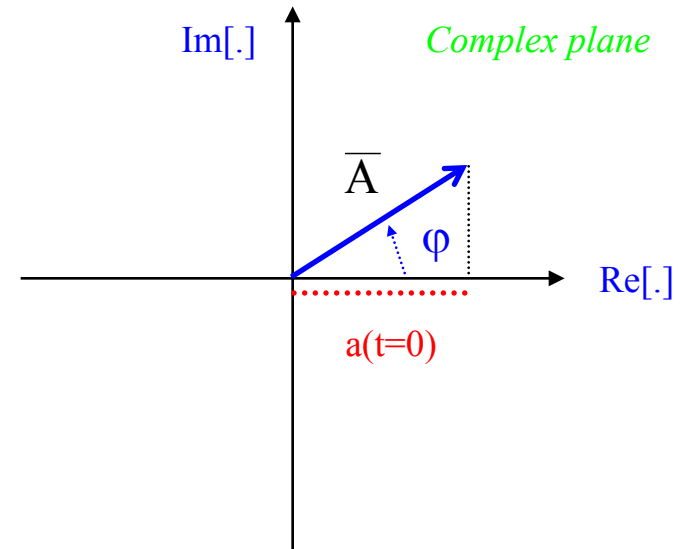
$$a(t) = \operatorname{Re}(A e^{j\varphi} e^{j\omega t})$$

with $e^{j\varphi} = \cos \varphi + j \sin \varphi$

$$\bar{A} = A e^{j\varphi}$$

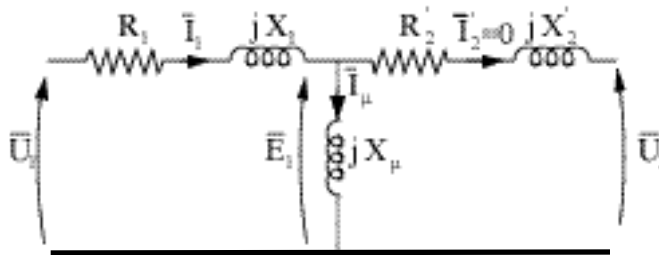
Quantity as a phasor

$$\begin{aligned} \operatorname{Re}(A e^{j\varphi} e^{j\omega t}) &= \operatorname{Re}(A e^{j\varphi + j\omega t}) = \operatorname{Re}(A e^{j(\omega t + \varphi)}) \\ &= \operatorname{Re}(A \cos(\omega t + \varphi) + j \sin(\omega t + \varphi)) \\ &= A \cos(\omega t + \varphi) \end{aligned}$$



Limit cases with phasors

No-load case



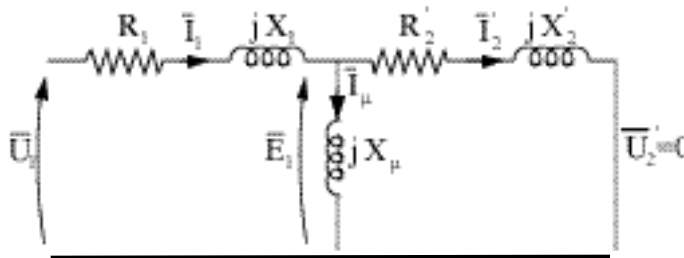
$$\bar{I}'_2 = 0 \Rightarrow \bar{U}'_2 = \bar{E}_1 = \frac{jX_\mu}{R_1 + jX_1 + jX_\mu} \bar{U}_1$$

$R_1, X_1 \ll X_\mu$ (ratios ~ 400 X, 4000 R)

$U'_2 \approx U_1 \Rightarrow \frac{U_1}{U_2} = n$

$$I_1 = I_\mu \ll I_{\text{nominal}}$$

Short-circuit case



$$\bar{U}'_2 = 0 \Rightarrow \frac{\bar{I}_1}{\bar{I}'_2} = \frac{R'_2 + jX'_2 + jX_\mu}{jX_\mu}$$

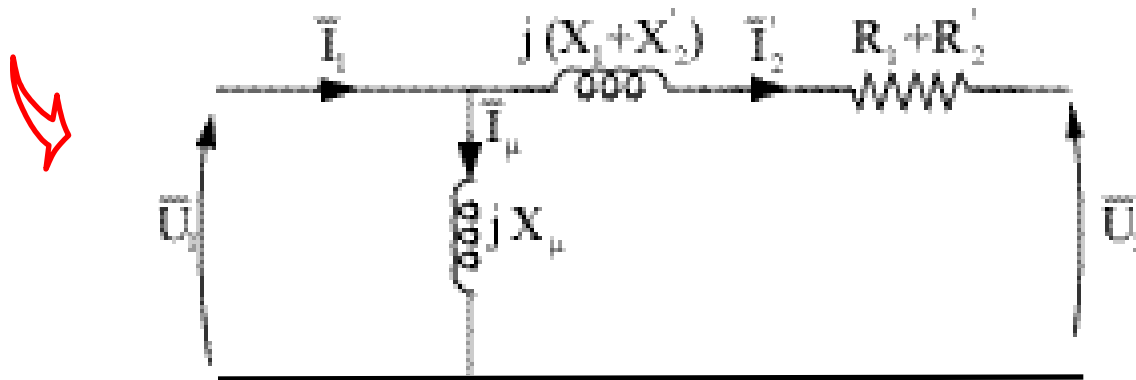
$R'_2, X'_2 \ll X_\mu$ (ratios ~ 400 X, 4000 R)

$I_1 \approx I'_2 \Rightarrow \frac{I_1}{I_2} = \frac{1}{n}$

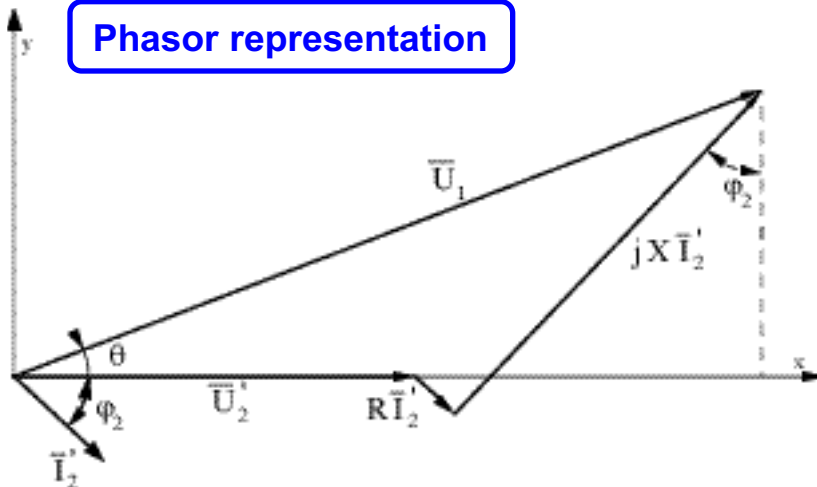
$$I_1 \gg !$$

Operating points

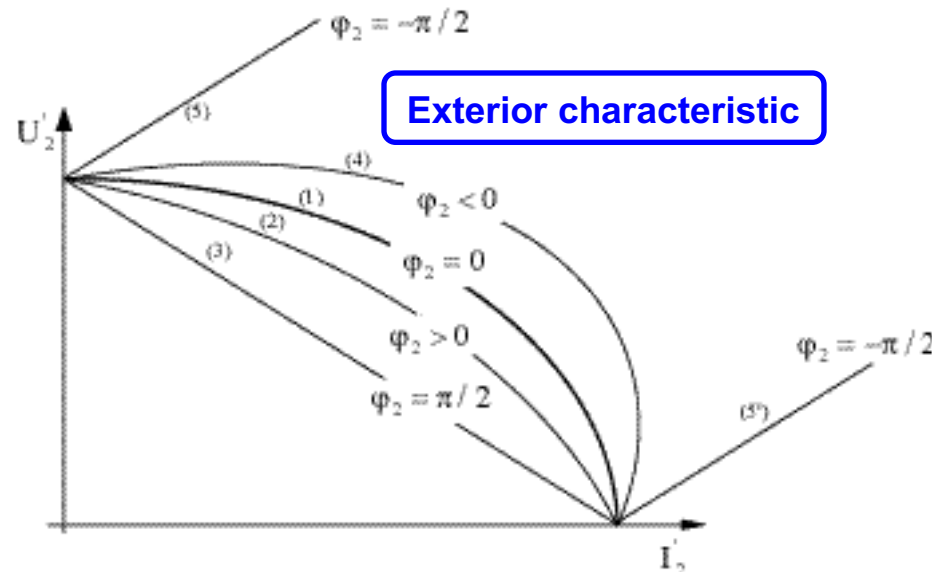
Simplified equivalent circuit



Phasor representation



Exterior characteristic



Magnetic losses and saturation

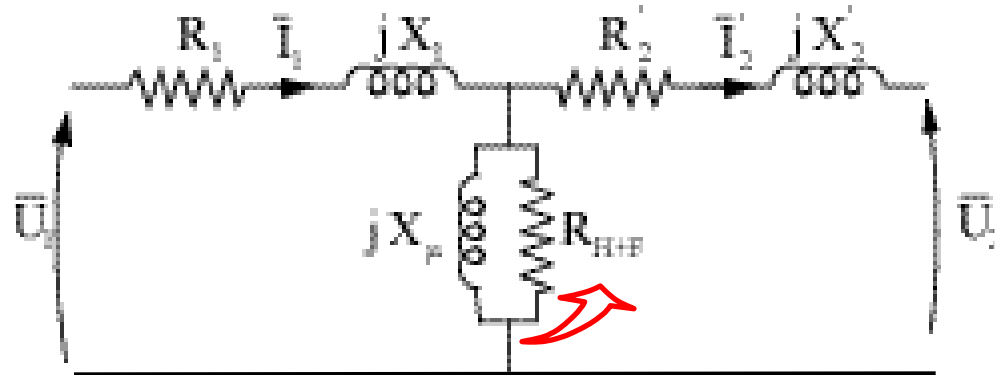
Hysteresis & eddy currents

Eddy current losses
proportional to b^2 , hence to Φ^2 , hence to E_1^2

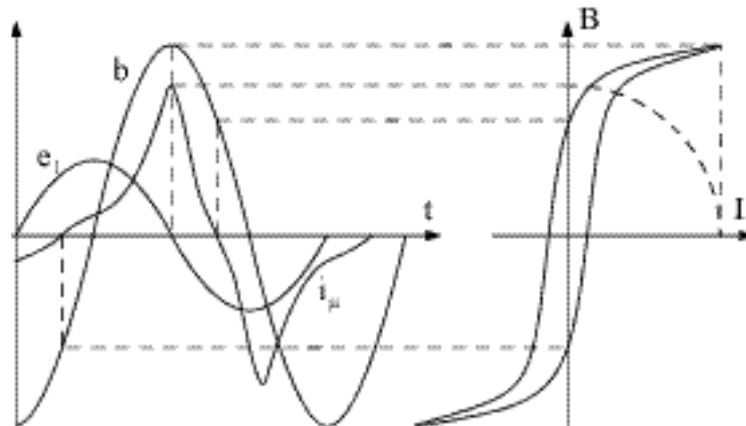
Idem for hysteresis losses (approx.)

$$p_{\text{mag}} = K_{\text{mag}} E_1^2 = \frac{E_1^2}{R_{\text{H+F}}}$$

(frequency dependent!)



Saturation



Equivalent circuit parameters

Experimental determination of the parameters
from the equivalent circuit

No-load test

$$I \ll \Rightarrow p_{\text{Joule primary}} \ll$$

$$P_v = \frac{U_1^2}{R_{H+F}}$$

$$Q_v = \frac{U_1^2}{X_\mu}$$

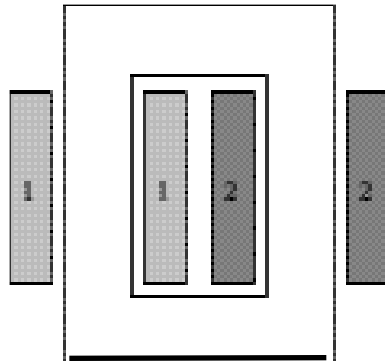
Short-circuit test

$$U_1 \ll \Rightarrow p_{\text{mag}} \ll$$

$$P_{cc} = (R_1 + R'_2) I_{cc}^2$$

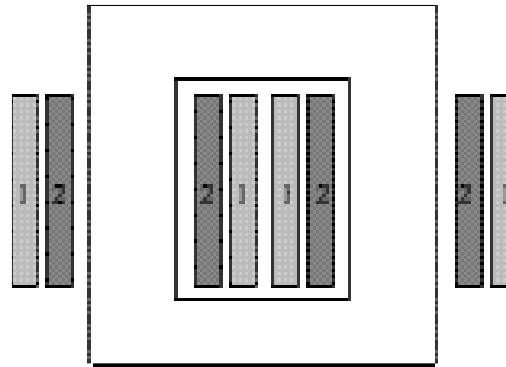
$$Q_{cc} = (X_1 + X'_2) I_{cc}^2$$

Construction types



Transformer with separate columns

High leakage flux

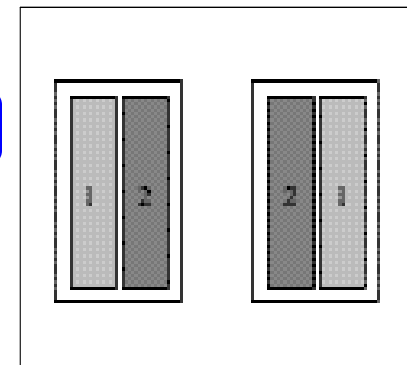


Transformer with concentric windings

Series or parallel connection of windings
1 : High Voltage, 2 : Low Voltage

Shell-type transformer (« cuirassé »)

1 : High Voltage, 2 : Low Voltage



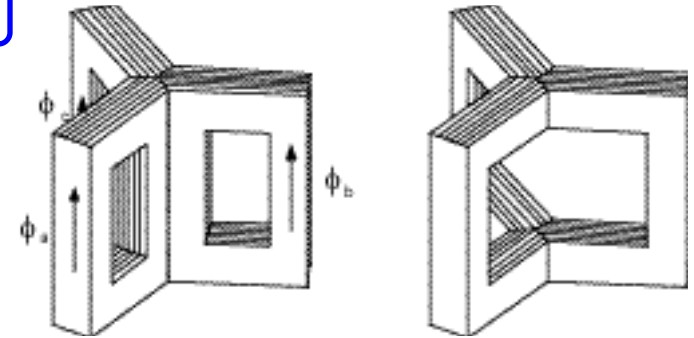
Three-phase transformer

3 single-phase transformer

advantages!

Geometric symmetry

3 primary windings and 3 secondary windings with star or triangle connection



$$\Phi_a + \Phi_b + \Phi_c = 0$$

Three columns

Five columns

Shell-type

